

Solution of problem # 16.1

$$f(z,t) = A \sin(kz) \cos(kvt)$$

$$\frac{\partial^2 f}{\partial z^2} = -Ak^2 \sin(kz) \cos(kvt)$$

$$\frac{\partial^2 f}{\partial t^2} = -Ak^2 v^2 \sin(kz) \cos(kvt) = v^2 \frac{\partial^2 f}{\partial z^2} \quad \checkmark$$

satisfies wave equation

$$\boxed{\frac{\partial^2 f}{\partial z^2} = \frac{1}{v^2} \frac{\partial^2 f}{\partial t^2}}$$

wave equation

Use trig identity $\sin \alpha \cos \beta = \frac{1}{2} [\sin(\alpha + \beta) + \sin(\alpha - \beta)]$ to

rewrite $f(z,t)$ as

$$\boxed{f(z,t) = \frac{A}{2} \left\{ \sin[k(z+vt)] + \sin[k(z-vt)] \right\}}$$

Two traveling waves, one moving to the left, the other to the right.

Solution of problem # 16.2

(a) $\vec{k} = -\frac{\omega}{c} \hat{x}$, $\hat{n} = \hat{z}$, $\vec{k} \cdot \vec{r} = -\frac{\omega}{c} x$, $\hat{k} \times \hat{n} = -\hat{x} \times \hat{z} = \hat{y}$

$$\vec{E}(x,t) = E_0 \cos\left(\frac{\omega}{c}x + \omega t\right) \hat{z} ; \quad \vec{B}(x,t) = \frac{E_0}{c} \cos\left(\frac{\omega}{c}x + \omega t\right) \hat{y}$$

(b) $\vec{k} = \frac{\omega}{c} \left(\frac{\hat{x} + \hat{y} + \hat{z}}{\sqrt{3}} \right)$, $\hat{n} = \frac{\hat{x} - \hat{z}}{\sqrt{2}}$ since \hat{n} is in the xz plane

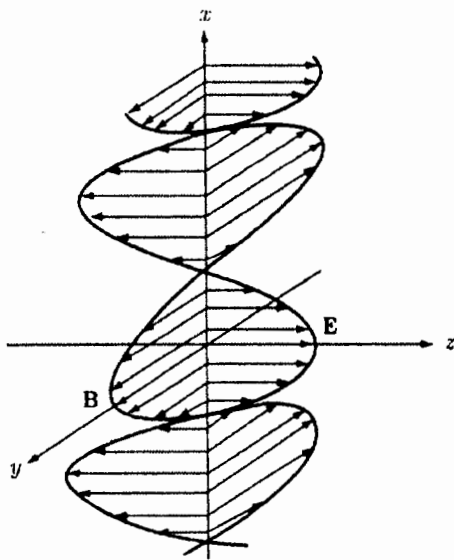
and it has to be perpendicular to \vec{k} .

$$\vec{k} \cdot \vec{r} = \frac{\omega}{\sqrt{3}c} (\hat{x} + \hat{y} + \hat{z}) \cdot (x\hat{x} + y\hat{y} + z\hat{z}) = \frac{\omega}{\sqrt{3}c} (x + y + z)$$

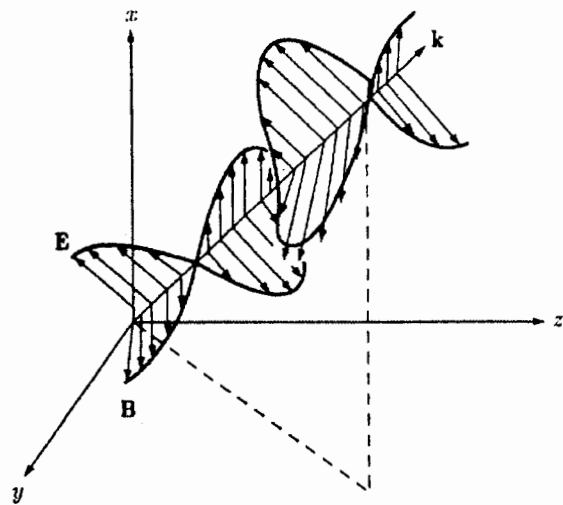
$$\hat{k} \times \hat{n} = \frac{1}{\sqrt{6}} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 1 & 1 & 1 \\ 1 & 0 & -1 \end{vmatrix} = \frac{1}{\sqrt{6}} (-\hat{x} + 2\hat{y} - \hat{z})$$

$$\vec{E}(x,y,z,t) = E_0 \cos\left[\frac{\omega}{\sqrt{3}c}(x+y+z) - \omega t\right] \left(\frac{\hat{x} - \hat{z}}{\sqrt{2}}\right)$$

$$\vec{B}(x,y,z,t) = \frac{E_0}{c} \cos\left[\frac{\omega}{\sqrt{3}c}(x+y+z) - \omega t\right] \left(\frac{-\hat{x} + 2\hat{y} - \hat{z}}{\sqrt{6}}\right)$$



(a)



(b)

Solution of problem # 16.3

Maxwell stress tensor:

$$T_{ij} = \epsilon_0 \left(E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right) + \frac{1}{\mu_0} \left(B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right)$$

$$\vec{E}(z, t) = E_0 \cos(kz - \omega t) \hat{x}, \quad \vec{B}(z, t) = \frac{1}{c} E_0 \cos(kz - \omega t) \hat{y}$$

Hence, all off-diagonal matrix elements vanish. For the diagonal elements we have

$$T_{xx} = \epsilon_0 \left(E_x E_x - \frac{1}{2} E^2 \right) + \frac{1}{\mu_0} \left(-\frac{1}{2} B^2 \right) = \frac{1}{2} \left(\epsilon_0 E^2 - \frac{1}{\mu_0} B^2 \right) = \frac{1}{2} \epsilon_0 (E^2 - E^2) = 0$$

$$T_{yy} = \epsilon_0 \left(-\frac{1}{2} E^2 \right) + \frac{1}{\mu_0} \left(B_y B_y - \frac{1}{2} B^2 \right) = \frac{1}{2} \left(-\epsilon_0 E^2 + \frac{1}{\mu_0} B^2 \right) = -\frac{1}{2} \epsilon_0 (E^2 - E^2) = 0$$

$$T_{zz} = \epsilon_0 \left(-\frac{1}{2} E^2 \right) + \frac{1}{\mu_0} \left(-\frac{1}{2} B^2 \right) = -\frac{1}{2} \left(\epsilon_0 E^2 + \frac{1}{\mu_0} B^2 \right) = -u$$

Hence, $T_{zz} = -\epsilon_0 E_0^2 \cos^2(kz - \omega t)$ and all other elements are zero.

The momentum of the fields is in the z -direction, and it is being transported in the z direction. Hence, it makes sense that T_{zz} is the only non-zero element in T_{ij} .

$-\vec{T} \cdot d\vec{a}$ is the rate at which momentum crosses an area $d\vec{a}$. Here there is no momentum crossing areas oriented in the x or y direction. The momentum per unit time per unit area flowing across a surface oriented in the z direction is $-T_{zz} = u = gc$. Hence, $\Delta p = gc A \Delta t$ and consequently $\Delta p / \Delta t = gc A =$ momentum per unit time crossing an area A .

Hence, evidently

$$\boxed{\text{momentum flux density} = \text{energy density}}$$

Solution of problem # 16.4

incoming fields:
$$\begin{cases} \vec{E}_I = \vec{E}_{0I} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)} \hat{y} \\ \vec{B}_I = \frac{1}{v_1} \vec{E}_{0I} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)} (-\cos\theta_1 \hat{x} + \sin\theta_1 \hat{z}) \end{cases}$$

reflected fields:
$$\begin{cases} \vec{E}_R = \vec{E}_{0R} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)} \hat{y} \\ \vec{B}_R = \frac{1}{v_1} \vec{E}_{0R} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)} (\cos\theta_1 \hat{x} + \sin\theta_1 \hat{z}) \end{cases}$$

transmitted fields:
$$\begin{cases} \vec{E}_T = \vec{E}_{0T} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)} \hat{y} \\ \vec{B}_T = \frac{1}{v_2} \vec{E}_{0T} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)} (-\cos\theta_2 \hat{x} + \sin\theta_2 \hat{z}) \end{cases}$$

(a) Boundary conditions: For $z=0$, $\vec{k}_I \cdot \vec{r} - \omega t = \vec{k}_R \cdot \vec{r} - \omega t = \vec{k}_T \cdot \vec{r} - \omega t$, so that we can drop all exponential factors in applying the boundary conditions.

Law of refraction: $\frac{\sin\theta_2}{\sin\theta_1} = \frac{v_2}{v_1}$

(i) $0=0$ (trivial, because $\vec{E} \perp \hat{z}$)

(iii) $\vec{E}_{0I} + \vec{E}_{0R} = \vec{E}_{0T}$ (since $\vec{E} \parallel \hat{y}$), $\vec{E}_{0I} + \vec{E}_{0R} = \vec{E}_{0T}$

(ii) $\frac{1}{v_1} \vec{E}_{0I} \sin\theta_1 + \frac{1}{v_1} \vec{E}_{0R} \sin\theta_1 = \frac{1}{v_2} \vec{E}_{0T} \sin\theta_2$ or $\vec{E}_{0I} + \vec{E}_{0R} = \frac{v_1 \sin\theta_2}{v_2 \sin\theta_1} \vec{E}_{0T}$; by the law of refraction then $\vec{E}_{0I} + \vec{E}_{0R} = \vec{E}_{0T}$ which is the same as (iii).

(iv) $\frac{1}{\mu_1} \left[\frac{1}{v_1} \vec{E}_{0I} (-\cos\theta_1) + \frac{1}{v_1} \vec{E}_{0R} \cos\theta_1 \right] = \frac{1}{\mu_2 v_2} \vec{E}_{0T} (-\cos\theta_2) \Rightarrow$

$$\vec{E}_{0I} - \vec{E}_{0R} = \frac{\mu_1 v_1}{\mu_2 v_2} \frac{\cos\theta_2}{\cos\theta_1} \vec{E}_{0T}$$

define

$\alpha = \frac{\cos\theta_2}{\cos\theta_1}, \beta = \frac{\mu_1 v_1}{\mu_2 v_2}$

$\vec{E}_{0I} - \vec{E}_{0R} = \alpha\beta \vec{E}_{0T}$

solution of 16.4 continues

We have to solve for \tilde{E}_{OR} and \tilde{E}_{OT}

$$\tilde{E}_{OT} = \frac{2}{1+\alpha\beta} \tilde{E}_{OI} \quad , \quad \tilde{E}_{OR} = \frac{1-\alpha\beta}{1+\alpha\beta} \tilde{E}_{OI}$$

Since α and β are positive it follows that \tilde{E}_{OT} and \tilde{E}_{OI} are in phase and the real amplitudes are related by

$$E_{OT} = \frac{2}{1+\alpha\beta} E_{OI}$$

The reflected wave is in phase if $\alpha\beta < 1$ and 180° out of phase if $\alpha\beta > 1$.

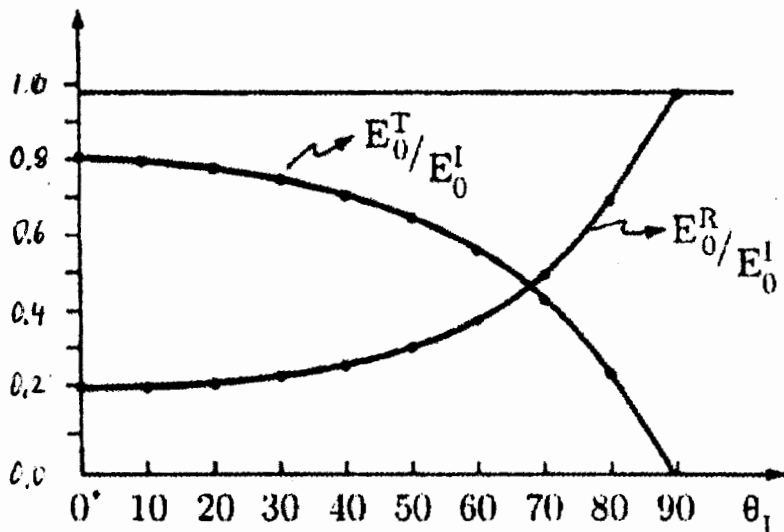
The real amplitudes are related by

$$E_{OR} = \left| \frac{1-\alpha\beta}{1+\alpha\beta} \right| E_{OI}$$

These are the Fresnel equations for polarization perpendicular to the plane of incidence.

(b) To construct the graphs, note that $\left(\beta \propto \frac{v_2}{v_1} = \frac{n_1}{n_2} \right)$

$$\alpha\beta = \beta \frac{\sqrt{1 - \sin^2 \theta_1 / \beta^2}}{\cos \theta_1} = \frac{\sqrt{\beta^2 - \sin^2 \theta_1}}{\cos \theta_1} = \frac{\sqrt{2.25 - \sin^2 \theta_1}}{\cos \theta_1}$$



(c) $E_{OR} = 0$ means $\alpha\beta = 1$ or $\alpha = \frac{\sqrt{1 - \left(\frac{v_2}{v_1}\right)^2 \sin^2 \theta}}{\cos \theta} = \frac{1}{\beta} = \frac{\mu_2 v_2}{\mu_1 v_1} = \frac{v_2}{v_1}$

Solution of problem # 16.4 continues

$$\text{or } 1 - \left(\frac{v_2}{v_1}\right)^2 \sin^2 \theta = \left(\frac{v_2}{v_1}\right)^2 \cos^2 \theta \quad \text{or } 1 \propto \left(\frac{v_2}{v_1}\right)^2. \text{ This can only be true}$$

for optically indistinguishable media, in which case there is of course no reflection, but this would be true at any angle and not just at the Brewster's angle.

S_R is either always 0 or always π for a given interface. S_R cannot switch over as θ is changed, the way it does for polarization in the plane of incidence.

(d) At normal incidence, $\alpha = 1$, and Fresnel's equations reduce to

$$E_{oT} = \frac{2}{1+\beta} E_{oI} \quad , \quad E_{oR} = \left| \frac{1-\beta}{1+\beta} \right| E_{oI} \quad , \quad \text{consistent with the results}$$

derived in class (note for normal incidence we cannot distinguish the cases of polarization parallel and perpendicular to the plane of incidence).

(e) Reflection and transmission coefficients:

$$R = \left(\frac{E_{oR}}{E_{oI}} \right)^2 = \left(\frac{1-\alpha\beta}{1+\alpha\beta} \right)^2 \quad , \quad T = \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \alpha \left(\frac{E_{oT}}{E_{oI}} \right)^2 = \alpha\beta \left(\frac{2}{1+\alpha\beta} \right)^2$$

$$R + T = \frac{1 - 2\alpha\beta + (\alpha\beta)^2 + 4\alpha\beta}{(1+\alpha\beta)^2} = 1 \quad \checkmark$$

Solution of problem #16.5

(a) Energy density of electromagnetic wave

$$u = \frac{1}{2} \left(\epsilon E^2 + \frac{1}{\mu} B^2 \right) = \frac{1}{2} e^{-2kz} \left[\epsilon E_0^2 \cos^2(kz - \omega t + \delta_E) + \frac{1}{\mu} B_0^2 \cos^2(kz - \omega t + \delta_E + \phi) \right]$$

Recall that in a conducting medium the electric and magnetic fields are no longer in phase. Time-averaging over a full cycle:

$$\langle u \rangle = \frac{1}{2} e^{-2kz} \left[\frac{\epsilon}{2} E_0^2 + \frac{1}{2\mu} B_0^2 \right]$$

We know that the ratio of the amplitudes is

$$\frac{B_0}{E_0} = \frac{k}{\omega} = \sqrt{\epsilon \mu \sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2}}, \quad k = |\tilde{k}|$$

so that

$$\langle u \rangle = \frac{1}{4} e^{-2kz} \epsilon E_0^2 \left[1 + \sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2} \right]$$

The real part of the complex wave number \tilde{k} is

$$k = \omega \sqrt{\frac{\epsilon \mu}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2} + 1 \right]^{1/2}}; \quad 1 + \sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2} = \frac{2}{\epsilon \mu} \left(\frac{k}{\omega} \right)^2$$

and

$$\boxed{\langle u \rangle = \frac{1}{4} e^{-2kz} \epsilon E_0^2 \frac{2}{\epsilon \mu} \left(\frac{k}{\omega} \right)^2 = \frac{k^2}{2\mu \omega^2} E_0^2 e^{-2kz}}$$

Hence, the ratio of the magnetic contribution to the electric contribution is

$$\frac{\langle u_{\text{mag}} \rangle}{\langle u_{\text{elec}} \rangle} = \frac{B_0^2 / \mu}{E_0^2 \epsilon} = \frac{1}{\epsilon \mu} \epsilon \mu \sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2} = \sqrt{1 + \left(\frac{\sigma}{\epsilon \omega} \right)^2} > 1 \quad \checkmark$$

$$(b) \quad \vec{S} = \frac{1}{\mu} (\vec{E} \times \vec{B}) = \frac{1}{\mu} E_0 B_0 e^{-2kz} \cos(kz - \omega t + \delta_E) \cos(kz - \omega t + \delta_E + \phi) \hat{z}$$

problem #16.5 continues

$$\langle \vec{S} \rangle = \frac{1}{\mu} E_0 B_0 e^{-2kz} \langle \cos^2(kz - \omega t + \delta_E) \cos \phi - \cos(kz - \omega t + \delta_E) \times \sin(kz - \omega t + \delta_E) \sin \phi \rangle \hat{z} = \frac{1}{2\mu} E_0 B_0 e^{-2kz} \cos \phi \hat{z}$$

Hence,
$$I = \frac{1}{2\mu} E_0 B_0 e^{-2kz} \cos \phi = \frac{1}{2\mu} E_0^2 e^{-2kz} \left(\frac{K}{\omega} \cos \phi \right),$$

but $k = K \cos \phi$, so that

$$I = \frac{k}{2\mu\omega} E_0^2 e^{-2kz}$$